

Constitutive model — isotropic damage model with linear softening (Mazars 1984)

$$\sigma = (1 - \omega)D : \epsilon$$
  
quiv. strain:  $\bar{\epsilon} = \sqrt{\sum_{I=1}^{3} \langle \epsilon_I \rangle^2} \quad \bar{\epsilon}_m(t) = \max_{t' \le t} \bar{\epsilon}$ 

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$$\omega = \begin{cases} 0 & \bar{\mathbf{\epsilon}}_m \leq f_t/E \\ 1 - \frac{f_t \left(2\gamma - f_t \bar{\mathbf{\epsilon}}_m\right)}{\bar{\mathbf{\epsilon}}_m \left(2\gamma E - f_t^2\right)} & f_t/E < \bar{\mathbf{\epsilon}}_m \leq 2\gamma/f_t \\ 1 & \text{otherwise} \end{cases}$$

Effective element width

## Simulated Strength Distributions — Effect of Element Size



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## Conclusions

- 1. Stochastic FE simulation of quasibrittle fracture requires special attention on how to numerically treat the strain localization phenomenon in a smeared continuum model.
- Two important aspects to consider: 1) regularization of fracture energy and 2) mesh-dependent strength distribution randomness in location of localization band.
- 3. The proposed probabilistic crack band model can effectively mitigate the mesh dependence of stochastic FE simulations, and can be potentially combined with fine-scale DEM model to form a multiscale analysis framework.

## Outlook

1. Extension of model to dynamic fracture — rate dependence on strength distribution function.



2. Stochastic simulations by directly using the random fields of material properties — mixture of different length scales: fracture length scale, auto-correlation lengths of different random fields.

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